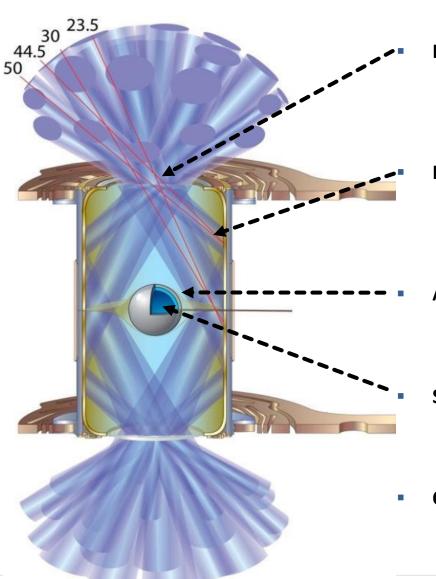
### Kinetic Physics in ICF Workshop: Discussion session – Day 3 – Theory

H.G. Rinderknecht, S. Wilks and P. Amendt Thursday, April 7, 1:30 pm



### Likely regions in ICF where kinetic physics may be important based on today's talks:



#### **LEH and laser/gas interactions**

Afeyan Hot electron generation, refluxing

#### Hohlraum gas/wall interface

Afeyan Hot electron generation, refluxing Simakov Interpenetration in stagnation

#### **Ablator**

Nonlocal e-xport Sunahara Orth Spallation?

#### Shock dynamics, hot spot assembly, burn

R. Mason Viscosity in shock front E. Vold Viscosity Olson Wetted foams Cohen KL physics

Other

### Questions to guide discussion:

- 1. Importance: How would this phenomenon impact the overall performance of an ICF implosion?
  - How would it impact observables?
  - What back-of-the-envelope calculation or test simulation supports the proposed impact(s)?

2. **Next Steps:** What proposed experiment or test problem would clearly demonstrate or benchmark this effect?



### 1. Quick overview of today's presentations on "Theory"

#### How important are these effects to ignition?

Landen: Evidence file ac ross NIF platforms and gauging of kinetic roles Mason: Real viscosity diffuses shock front, but how is ignition margin affected? Flux limit sensitivity to multiple cells? Testable? Rosenberg EP's already? Other viscosity models? Why is B 2x larger with viscosity despite smoothing?

Vold: xRage applied to pair of Omega shots shows qualitative agreement and consistent with Ho/Zimmerman results. Less convergence from viscosity => less Pstag?

Sunahara: Spark experiment shows interpenetrating flows; modeling in progress with DSMC Langevin model. Nonlocal xport important for DD. Is time-dependent flux multiplier needed in ID?

Afeyan: Exploit LPI to understand kinetics, measure space and time varying hots, measure vdf's.

Simakov: Plasma rad-hydro transport model includes O(Kn) effects. Same physics as in xRage? Impact on ignition margins?

Cohen: Kinetics matter, but KL tail effect on fusion reaction rate is small.

Kagan: Simple kinetics model might explain DD vs DT Ti anomaly using local Kn from hot-spot boundary perturbations. Extended kTi from tenuous plasma to strong



### 1. Quick overview of today's presentations on "Theory"

How important are these effects to ignition?

Olson: Wetted foam+fuel platform can span Kn's for kinetic to fluidlike regime!

Orth: Delay in phase transition behind first shock may seed RT/RM at fuel/pusher interface (scale size?); testable on Omega/NIF? Role for MD simulations to constrain phase transition time scale? Vary grain size in 1D slab experiments on OMEGA?



## Electron and ion thermo-diffusion may be greatly enhanced in high-Z hohlraums filled with low-Z gas

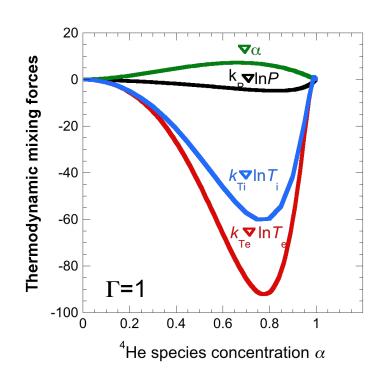
#### **HOHLRAUM DIFFUSION**

$$i = -\rho D \cdot (\nabla \alpha + k_P \nabla \ln P + k_{T_e} \nabla \ln T_e + k_{T_i} \nabla \ln T_i + k_V \nabla^2 v)$$
 Kagan and Tang, Phys. Lett. **A 378**, 1531 (2014)

$$\nabla \ln T = \nabla \ln P \left( \frac{\gamma - 1}{\gamma} \right) + \frac{\Delta Z}{\bar{Z} + \Gamma^{-1}} \frac{m_1}{m_2}$$

$$\times \frac{\nabla \alpha}{[\alpha + (1 - \alpha)m_1/m_2]^2},$$

Amendt, Bellei and Wilks, PRL 109, 075002 (2012)



- Large ΔZ can promote temperature inversion within mix layer, potentially leading to throttled e<sup>-</sup> transport and reduced drive
- Local approximation for T,P profiles does not apply to strong shocks



#### THEORY RESULTS SUMMARY

- Real viscosity in simulations shows deviations from inviscid results
- Self-consistent inclusion of plasma transport in fluid models may help to understand heating/stagnation phenomena in hohlraums/capsules
- Phase transition delay in strong shocks in ablator may eject material from ablator into ice
- Wetted foam platform on the NIF provides knob on Kn through gas density
- Variable convergence Symcaps with hydro-equivalent DD, D3He fill could provide another Kn platform: Does Rygg anomaly exist on the NIF?
- Hot electron anisotropy could seed non-uniform burn
- Global KL physics doesn't appear to greatly affect burn, but locally large Kn pockets from instability may have important effect
- Resistive heating from time-varying (converging) shock in gaseous fuel?
- Does enthalpy of mix contribute to low DSR's?



#### THEORY ACTION ITEMS

- Quantitatively assess impact of viscosity on ignition: devise test of simulations
- Understand limits of mass diffusive flux expression especially for strong shocks
  - Impact on energy transport
- Spallation from 1<sup>st</sup> shock in solid ablator: Design Omega experiment to test
- Design Hy-Eq Symcap platform to dial in kinetic effects
- Hot electron anisotropy could seed non-uniform burn: Quantify
- Assess upper bound on possible resistive heating in fuel
- Does enthalpy of mix contribute to low DSR?
- Hohlraum/gas interface mix from ion diffusion or hydro-instability: does it play a role on missing energy / multipliers?



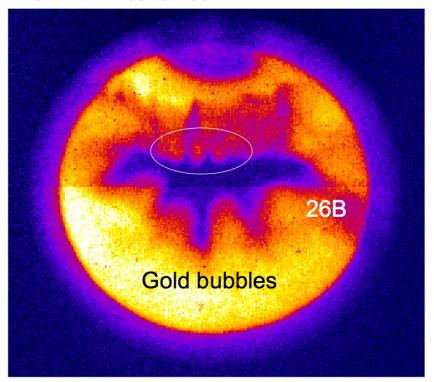
#### THEORY ACTION ITEMS

- Quantitatively assess impact of viscosity on ignition: devise test of simulations
- Understand limits of mass diffusive flux expression especially for strong shocks
  - Impact on energy transport, e.g., from LL:  $q = [k_T(\partial \mu / \partial c)|_{P,T} T(\partial \mu / \partial T)|_{P,c} + \mu]i k\nabla T$
- Spallation from 1<sup>st</sup> shock in solid ablator: Design Omega experiment to test
- Design Hy-Eq Symcap platform to dial in kinetic effects
- Hot electron anisotropy could seed non-uniform burn: Quantify
- Assess upper bound on possible resistive heating in fuel
- Does enthalpy of mix contribute to low DSR?
- Hohlraum/gas interface mix from ion diffusion or hydro-instability: does it play a role on missing energy / multipliers?
- Local Kn physics in hot spot and effects on ion temperature measurements

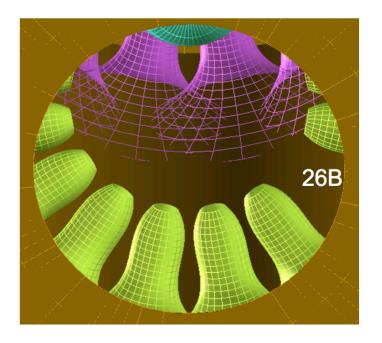


# The plasma bubbles correlate with the beam locations, and the instability features are near the root of the outer beams (courtesy of Hui Chen)

GLEH: N160202-004



Visrad: N160202-004 (GLEH view)



Gold bubbles grow at 50um/ns to about 2 mm out of the hohlraum wall.

### Species separation in planar steady shock wave replicates thermodynamic force terms, if Péclet number is large

- Planar steady shock wave in binary mixture
- Solution to continuity equation for mass fraction c of light species

$$c(x) \cong c_{+} + \frac{F(x)L_{i}}{R_{+}(x)Pe(x)} - \sum_{n=1}^{\infty} \frac{L_{i}^{n+1}}{\left[-R_{+}(x)Pe(x)\right]^{n+1}} \frac{d^{n}F(x)}{dx^{n}}$$

where

 $c_{\perp}$  = mass fraction in unshocked material

F(x) is thermodynamic force:

$$F(x) = k_P(c(x)) \frac{d \log P_i}{dx} + k_E(c(x)) \frac{T_e}{T_i} \frac{d \log \rho}{dx} + k_T^{(i)}(c(x)) \frac{d \log T_i}{dx} + k_T^{(e)}(c(x)) \frac{d \log T_e}{dx}$$

Pe(x) is Péclet number:  $Pe(x) = u_{+}L_{i}/D(x)$ , where  $u_{+}$  is shock velocity,  $L_{i}$  is shock width,

D(x) is diffusivity,  $R_{+}(x)$  is (compression)<sup>-1</sup> =  $\rho_{+}/\rho(x)$ 

When Pe is large,

$$c(x) \approx c_+ + \frac{F(x)L_i}{R_+(x)Pe(x)}$$

Expression is suggested by solution to approximate linear ODE with constant coefficients



neon mass fraction

shock

scaled thermodynamic

force terms

15 ns

0.20

0.15

0.10 -

0.05

# C. Orth preliminary proposal — Add phase nucleation & spallation to target design codes

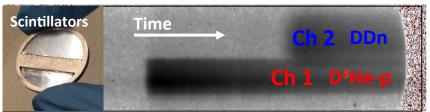
- When a ≥1 Mbar-level shock transits ablator material still in a solid phase (e.g., as determined by its temperature or MJ/kg), keep it in the solid phase for another ∆t ps (e.g., don't let it expand). This is secondary.
  - Work with Orth to determine  $\Delta t$  (~200 ps?).
- If the shock transit of a solid region is adjacent to the fuel, make the solid spall according to the following reference, delay the shock propagating further by  $\Delta t$  ps, and roughen the surface according to the expected size of the spalled chunks (1, 10, and 14 microns respectively for HDC, sintered Be, and GDP-CH).
  - This is primary (and not easy).
  - C. Orth, Physics of Plasmas, 23, 022706-1 (2016).

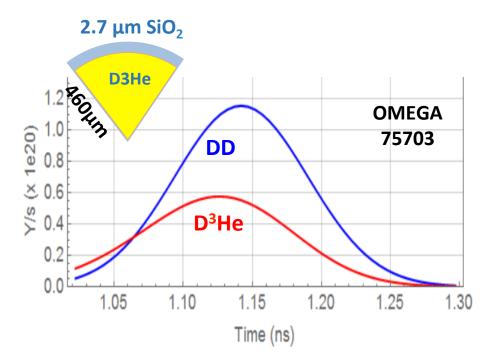
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# High-precision measurements of multiple nuclear burn histories to probe time evolution of species separation in kinetic to hydro-like 1D plasmas

#### PXTD streak image of DD and D<sup>3</sup>He signal





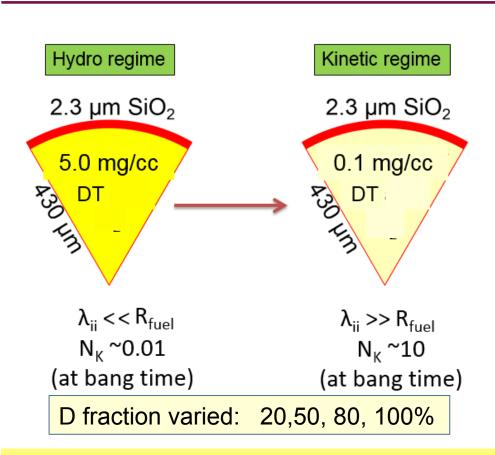
#### **Additional measurements:**

- Yield(DD) and Yield(D³He)
- Tion(DD) and Tion(D<sup>3</sup>He)
- Te
- DD and D<sup>3</sup>He burn profiles
- R(t)
- Convergence
- ρR<sub>fuel</sub> and ρR<sub>tot</sub>

#### Physics motivation:

To quantify the instantaneous rate of species separation in implosions

## DT exploding pushers at OMEGA will be used to explore the transition between hydro/multi-fluid to kinetic regimes



### **Measured quantities on one DT shot:**

Yield (DD) and Yield (DT) Tion(DD) and Tion(DT) Te DT and DT burn histories DT and DD burn profiles R(t) Convergence  $\rho R_{\text{fuel}}$  and  $\rho R_{\text{shell}}$ 

#### PHYSICS MOTIVATION:

Simplest possible implosions with extensive precision diagnostics, **leaving no wiggle room**, that can be compared in detail to fluid, hybrid, and kinetic simulations.

**RELEVANCE**:, hot-spot ignition (shock convergence), wetted foam, shock ignition, species separation, species temperature disequilibrium, ....

### Recent work is assessing enthalpy of mixing in HDC implosions and gas-filled hohlraums

#### **ENTHALPY OF MIX**

• Temperature and pressure differences between two contiguous vessels with distinguishable particles drives enthalpy change (*H*=*E*+*PV*)

$$\Delta H = Nk_B T' \ln \left[ \left( \frac{P_1}{P'} \left( \frac{T'}{T_1} \right)^{c_P/k_B} \right)^c \cdot \left( \frac{P_2}{P'} \left( \frac{T'}{T_2} \right)^{c_P/k_B} \right)^{1-c} \right], \quad \text{where}$$

$$\frac{1}{P'} = \left[ \frac{cT_1}{P_1} + \frac{(1-c)T_2}{P_2} \right] \cdot \frac{1}{cT_1 + (1-c)T_2}, \qquad T' = \frac{N_1T_1 + N_2T_2}{N_1 + N_2},$$

- Pressure gradient scale length often well exceeds temperature gradient scale length, leading to isobaric approximation
  - $\Delta H = \Delta Q$  and  $\Delta E = \Delta H P dV$



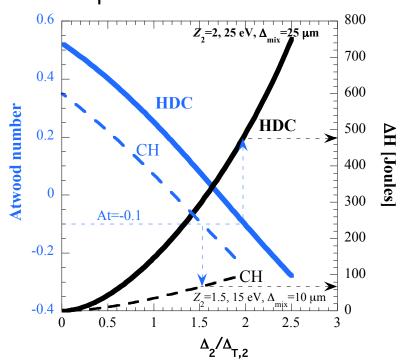
# Recent work is assessing enthalpy of mixing in HDC implosions and finds potential several hundred J of $\Delta H$

#### **ENTHALPY OF MIX**

• Under quasi-isobaric conditions we can solve for the Atwood number on the DT ice/pusher interface for a parameterized temperature ratio

$$At = \frac{\frac{A_2}{1 + Z_2} - \frac{A_1}{1 + Z_1} \cdot \left(\frac{T_2}{T_1}\right)}{\frac{A_2}{1 + Z_2} + \frac{A_1}{1 + Z_1} \cdot \left(\frac{T_2}{T_1}\right)} \qquad \frac{T_2}{T_1} \cong \frac{1 + \frac{\Delta_2}{2\Delta_{T,2}}}{1 - \frac{\Delta_1}{2\Delta_{T,1}}}$$

• For a temperature ratio free of resonance at  $\Delta_1$ =2 $\Delta_{T,1}$ , e.g., (1+tanh)/(1-tanh),  $\Delta H$  for HDC is ~ 200 J



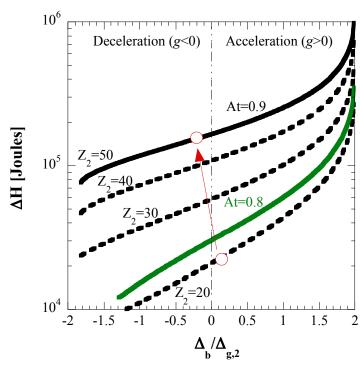
# Recent work is assessing enthalpy of mixing in gas-filled hohlraums and finds nearly 100 kJ of $\Delta H$

#### **ENTHALPY OF MIX**

 For given normalized bubble size and Atwood number, ratio of temperatures is used to evaluate DH

$$\frac{T_2}{T_1} = \frac{\left[1 + \frac{2\Delta_b}{\Delta_{g,2}} \left(\frac{1 - At}{1 + At}\right)^{0.66} \left(1 - \frac{\Delta_b}{2\Delta_{g,2}}\right)\right]^{1/2} - 1}{\frac{\Delta_b}{\Delta_{g,2}} \left(\frac{1 + At}{1 - At}\right)^{0.34} \frac{1 + Z_2}{1 + Z_1} \frac{A_1}{A_2}}.$$

 ΔH between end of low foot to peak power exceeds 100 kJ for Z<sub>Au</sub>=50, At=0.9



# Currents are generated in converging shocks in ICF fuels, leading to Joule heating not captured in mainline codes

#### **JOULE HEATING**

• Shock front electric field E scales as:  $E \cong k_B T / e \Delta_s \equiv k_B T / e \eta_\infty \lambda_{mfp}$ 

- Ion mean free path scales as  $T^2/n$ , giving:  $E \cong k_B T / e \eta_\infty \lambda_{mfp} \propto n / T$ 
  - Converging shocks in fuel reach Mach number near 50, so that  $E \rightarrow 0$  near center at shock flash
  - Consequently, *E* is strong function of time during shock transit
- Ampere's Law gives:  $\int dV \int dt \ \vec{j} \cdot \vec{E} \cong -\int dV \int dt \cdot \partial_t E^2 / 8\pi \equiv V \left\langle E^2 / 8\pi \right\rangle_{Volume}$

# Currents are generated in converging shocks in ICF fuels, leading to Joule heating not captured in mainline codes

#### **JOULE HEATING**

• For Rev.5 CH design (4 shocks):

$$\left\langle \frac{E^2}{8\pi} \right\rangle [erg/cm^3] = \frac{118 \cdot 16^4 \rho_0^2 [mg/cm^3] \ln^2 \Lambda}{T_e^2 [keV] \eta_\infty^2},$$

• Using  $\rho_0$ =0.4 mg/cm³, ln $\Lambda$ =10,  $\overline{T}_e$ =0.1 keV, V=0.002 cm³, we find several Joules of resistive heating in gaseous fuel

 Increase in fuel pressure at deceleration onset leads to decrease in stagnation pressure of ~30-40% from adiabatic implosion model



## Electron and ion thermo-diffusion may be greatly enhanced in high-Z hohlraums filled with low-Z gas

#### **HOHLRAUM DIFFUSION**

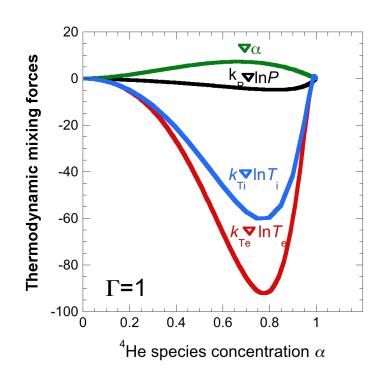
$$i = -\rho D \cdot (\nabla \alpha + k_P \nabla \ln P + k_{T_e} \nabla \ln T_e + k_{T_i} \nabla \ln T_i + \ldots)$$

Kagan and Tang, Phys. Lett. A 378, 1531 (2014)

$$abla \ln T = 
abla \ln P \left( \frac{\gamma - 1}{\gamma} \right) + \frac{\Delta Z}{\bar{Z} + \Gamma^{-1}} \frac{m_1}{m_2}$$

$$\times \frac{\nabla \alpha}{[\alpha + (1 - \alpha)m_1/m_2]^2},$$

Amendt, Bellei and Wilks, PRL 109, 075002 (2012)



• Large ΔZ can promote temperature inversion within mix layer, potentially leading to throttled e<sup>-</sup> transport and reduced drive

